

L05-07: Reflection and Transmission from Interfaces

EE3109 Applied Electromagnetics

Lecture Notes

Dr. Alex M. H. Wong

Jan – Apr 2023

Outline

- Course Matter
- Reflection and Transmission
- Normal Incidence
- Oblique Incidence

Announcements (Lecture 5)

- Test 1 Details
 - Date and Time: Feb 23rd, **3:15-4:15pm**
 - **Location: CMC M5050 (Note Unusual Building)**
 - Coverage: Up to and including L04a and the corresponding tutorial material
 - 1 A4-Sized Aid Sheet Allowed
- L06 Location
 - We will stay in the lecture hall **CMC M5050** for L06 after the class ends
- Asst 1B due today
- Asst 1B Sol'n Availability Time
- Conceptual Questions CQ01-CQ03

Announcements (Lecture 7)

- Discussion on test mitigation
 - As per University and Department regulation, mitigation will not be allowed for assessment activities that make up for less than 20% of the total grade. Students missing such assessments (even for legitimate reasons) will receive a grade of zero for the assessment.
 - A special case was invoked for Test 1. The above regulation will be in enforced for Test 2.
- Lab 1 Starts on Week 9
 - Lab 1: Lau (AC3) 15th Floor; Lab 2: Yeung (AC1) P1615
 - Session 1: Weeks 10 & 12, Wed 9am - 12nn (31 students)
 - Session 2: Weeks 9 & 11, Wed 9am - 12nn (32 students)
 - Session 3: **Weeks 9 & 11**, Fri 7pm - 10pm (11 students)
- Asst 2 Posted, Due in Week 9

Tentative Course Schedule

Week #	Week of	Course Coverage
1	Jan 9	Course Introduction, Math Review
2	Jan 16	Introduction to Maxwell Equations, Materials and Boundaries
	Jan 23	<i>Happy Chinese New Year!</i>
3	Jan 30	Wave Equations, Plane Waves, Propagation in Lossy Media
4	Feb 6	Polarizations, <i>Asst. 1a Due</i>
5	Feb 13	EM Potential, Polarizations Cont'd, Potentials <i>Asst. 1b Due</i>
6	Feb 20	Test 1 , Reflection and Transmission
7	Feb 27	Reflection and Transmission Cont'd, Poynting vector, Power
8	Mar 6	Power, Velocity, Waveguides and Transmission Lines (TL)
9	Mar 13	VIP in a TL, Terminated and Lossy TLs, <i>Asst. 2 Due, Lab 1 Begins</i>
10	Mar 20	Impedance in a TL, Smith Charts,
11	Mar 27	Smith Charts Cont'd, Impedance Matching, Quarter-wave Transformers, <i>Lab 2 Begins</i>
12	Apr 3	Test 2 , Introduction to Antennas
13	Apr 10	Dipole Antennas, <i>Asst. 3 Due</i>

Review and Preview

- Up till now, we talked about
 - Maxwell's equations, waves equations, potentials
 - Plane waves and its properties (amplitude, phase, directions, polarization, frequency and wavelength)
 - Plane wave propagation in lossless and lossy media
- This class, we will look at
 - How the plane wave behaves in the presence of a material interface

Big Picture: Signal Refraction at Boundaries

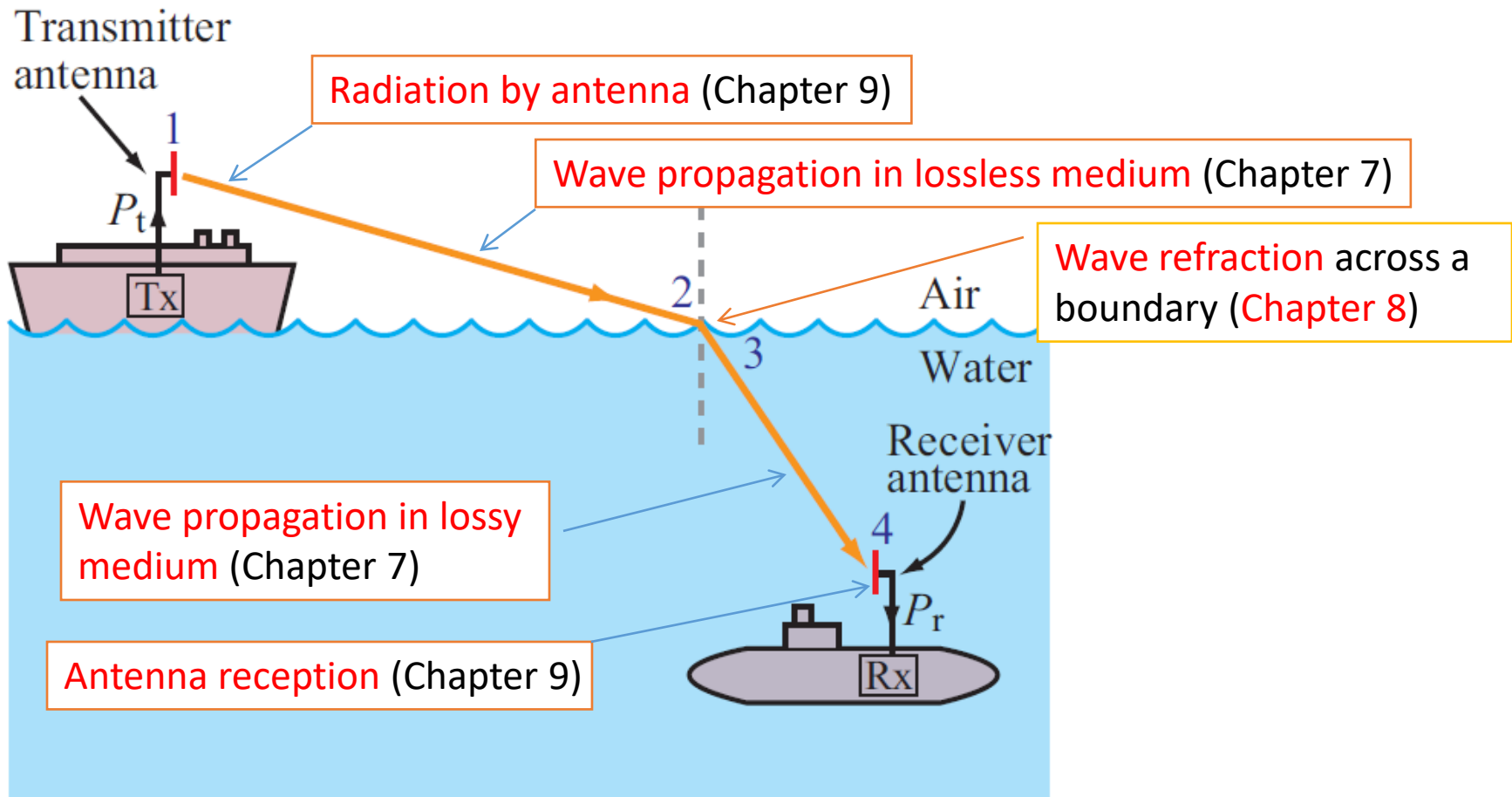
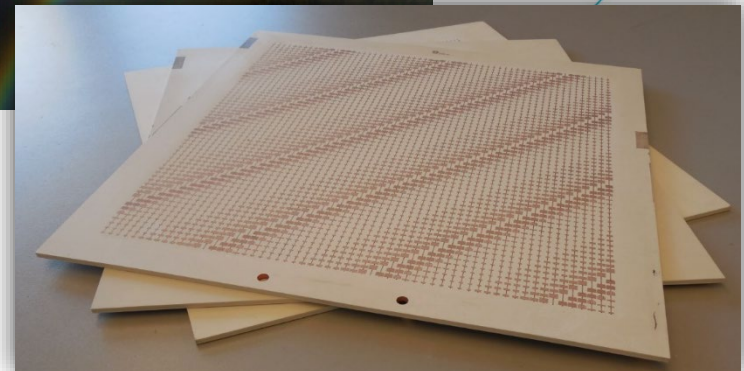
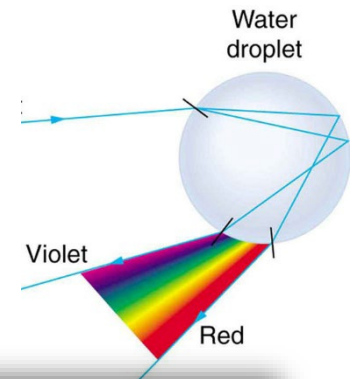
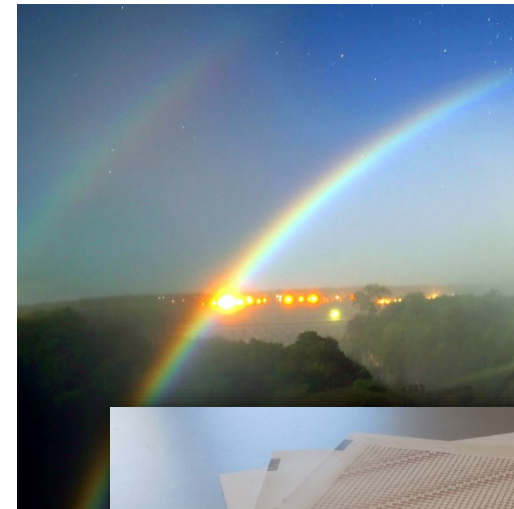
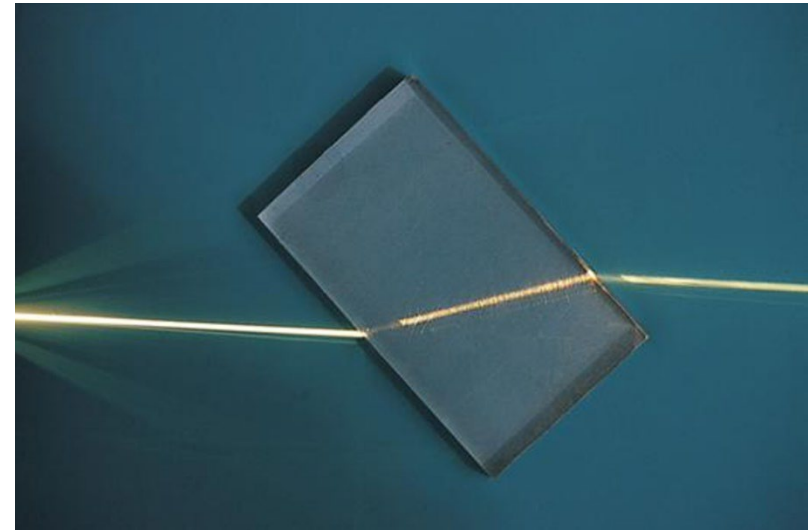


Figure 8-1: Signal path between a shipboard transmitter (Tx) and a submarine receiver (Rx).

Outline

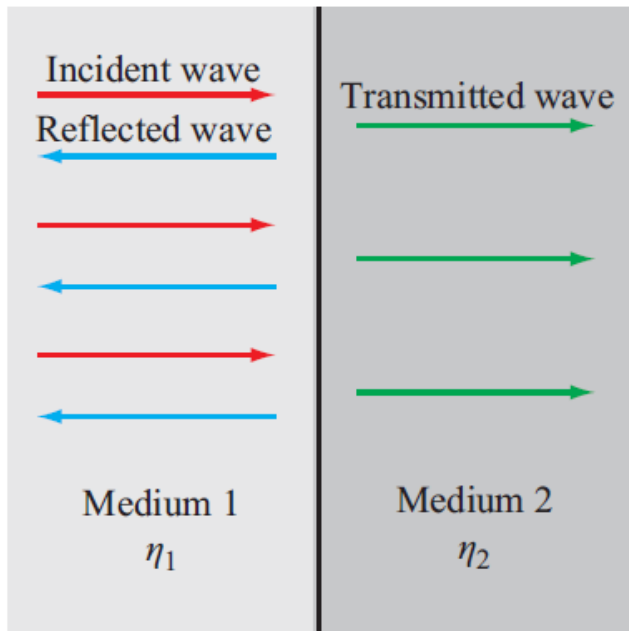
- Course Matter
- Reflection and Transmission
- Normal Incidence
- Oblique Incidence

Examples of EM Wave Reflection and Transmission

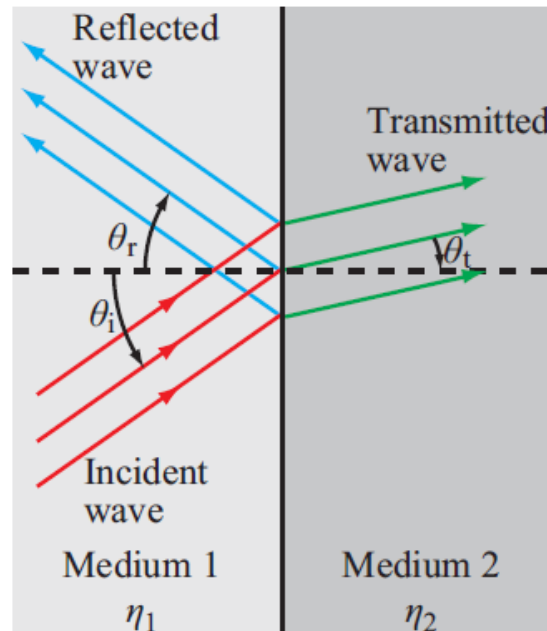


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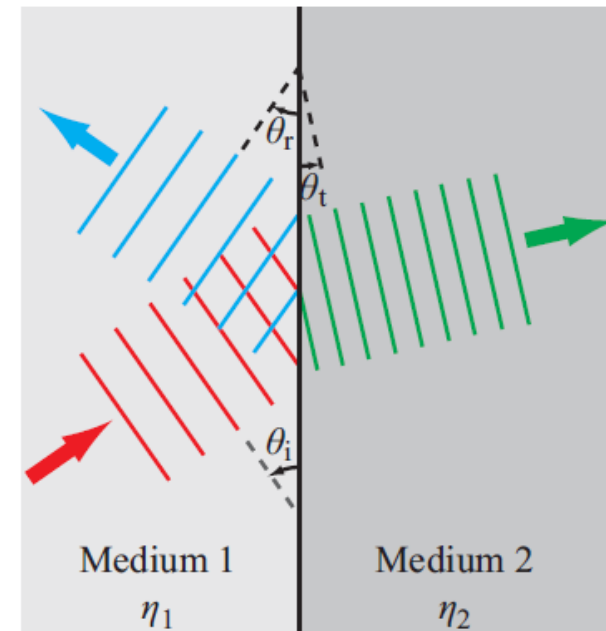
Normal and Oblique Incidence



(a) Normal incidence

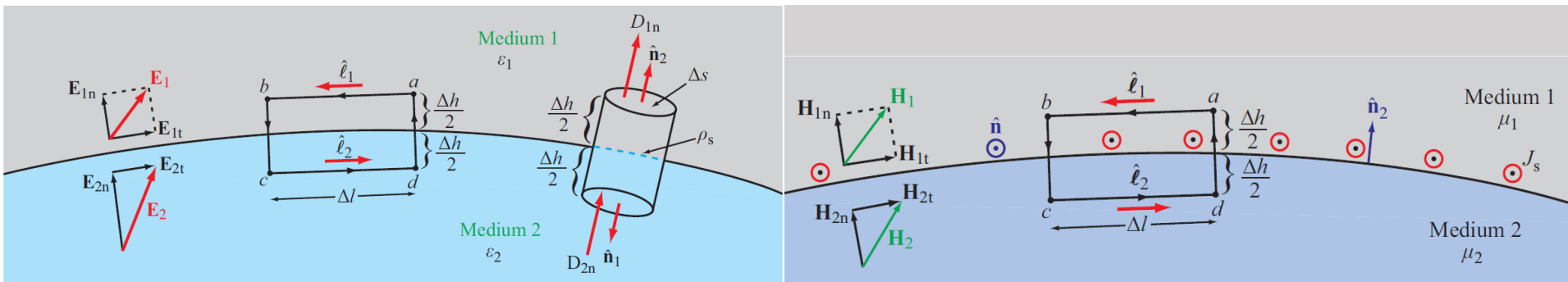


(b) Ray representation of oblique incidence



(c) Wavefront representation of oblique incidence

Review: Electromagnetic BCs



Tangential Components:

$$\mathbf{E}_{1t} = \mathbf{E}_{2t} ; \mathbf{H}_{1t} - \mathbf{H}_{2t} = \mathbf{J}_s$$

Normal Components:

$$\mathbf{D}_{1n} - \mathbf{D}_{2n} = \rho_s ; \mathbf{B}_{1n} = \mathbf{B}_{2n}$$

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Individual Waves

Incident Wave

$$\tilde{\mathbf{E}}^i(z) = \hat{\mathbf{x}} E_0^i e^{-jk_1 z},$$

$$\tilde{\mathbf{H}}^i(z) = \hat{\mathbf{z}} \times \frac{\tilde{\mathbf{E}}^i(z)}{\eta_1} = \hat{\mathbf{y}} \frac{E_0^i}{\eta_1} e^{-jk_1 z}.$$

Reflected Wave

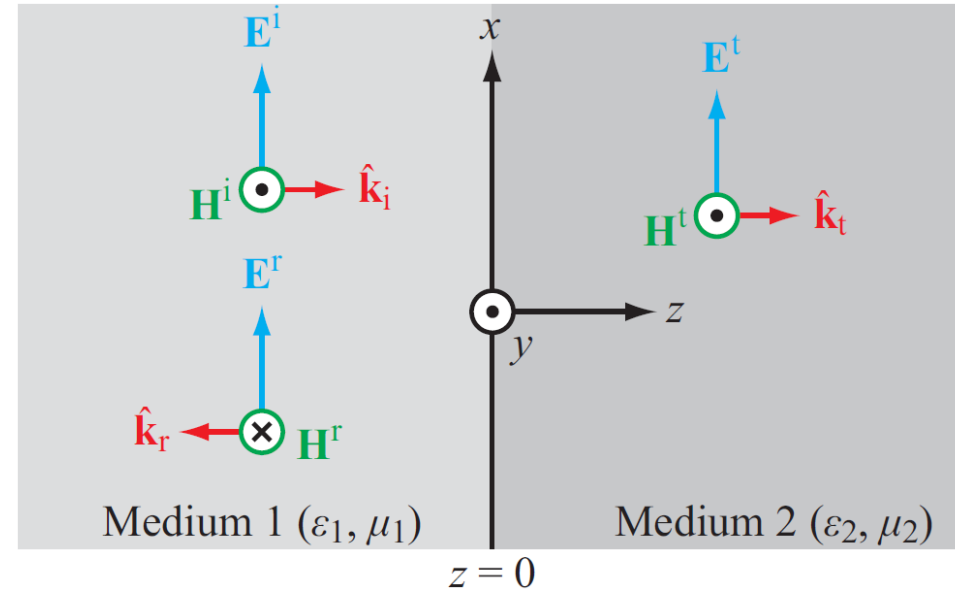
$$\tilde{\mathbf{E}}^r(z) = \hat{\mathbf{x}} E_0^r e^{jk_1 z},$$

$$\tilde{\mathbf{H}}^r(z) = (-\hat{\mathbf{z}}) \times \frac{\tilde{\mathbf{E}}^r(z)}{\eta_1} = -\hat{\mathbf{y}} \frac{E_0^r}{\eta_1} e^{jk_1 z}.$$

Transmitted Wave

$$\tilde{\mathbf{E}}^t(z) = \hat{\mathbf{x}} E_0^t e^{-jk_2 z},$$

$$\tilde{\mathbf{H}}^t(z) = \hat{\mathbf{z}} \times \frac{\tilde{\mathbf{E}}^t(z)}{\eta_2} = \hat{\mathbf{y}} \frac{E_0^t}{\eta_2} e^{-jk_2 z}.$$



Note – sign

Note + sign

Note – sign

Add in Boundary Conditions

Total fields

Medium 1

$$\begin{aligned}\tilde{\mathbf{E}}_1(z) &= \tilde{\mathbf{E}}^i(z) + \tilde{\mathbf{E}}^r(z) \\ &= \hat{\mathbf{x}}(E_0^i e^{-jk_1 z} + E_0^r e^{jk_1 z}),\end{aligned}\quad (8.4a)$$

$$\begin{aligned}\tilde{\mathbf{H}}_1(z) &= \tilde{\mathbf{H}}^i(z) + \tilde{\mathbf{H}}^r(z) \\ &= \hat{\mathbf{y}} \frac{1}{\eta_1} (E_0^i e^{-jk_1 z} - E_0^r e^{jk_1 z}).\end{aligned}\quad (8.4b)$$

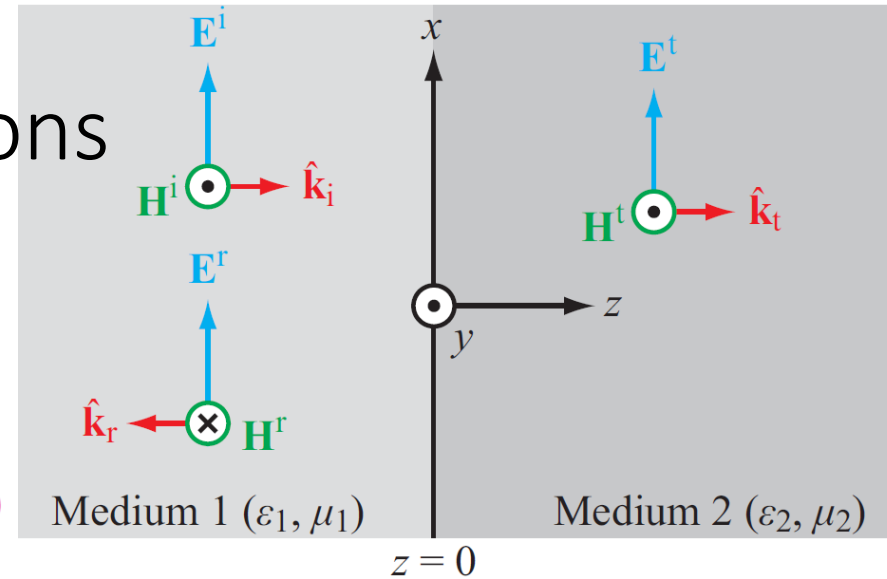
Medium 2

$$\tilde{\mathbf{E}}_2(z) = \tilde{\mathbf{E}}^t(z) = \hat{\mathbf{x}} E_0^t e^{-jk_2 z}, \quad (8.9a)$$

$$\tilde{\mathbf{H}}_2(z) = \tilde{\mathbf{H}}^t(z) = \hat{\mathbf{y}} \frac{E_0^t}{\eta_2} e^{-jk_2 z}. \quad (8.9b)$$

At the boundary $z = 0$:

$$\begin{aligned}\tilde{\mathbf{E}}_1(0) &= \tilde{\mathbf{E}}_2(0) \quad \text{or} \quad E_0^i + E_0^r = E_0^t, \\ \tilde{\mathbf{H}}_1(0) &= \tilde{\mathbf{H}}_2(0) \quad \text{or} \quad \frac{E_0^i}{\eta_1} - \frac{E_0^r}{\eta_1} = \frac{E_0^t}{\eta_2}.\end{aligned}$$



Solution gives:

$$E_0^r = \left(\frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} \right) E_0^i = \Gamma E_0^i,$$

$$E_0^t = \left(\frac{2\eta_2}{\eta_2 + \eta_1} \right) E_0^i = \tau E_0^i,$$



$$\begin{aligned}\Gamma &= \frac{E_0^r}{E_0^i} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} \quad (\text{normal incidence}), \\ \tau &= \frac{E_0^t}{E_0^i} = \frac{2\eta_2}{\eta_2 + \eta_1} \quad (\text{normal incidence}).\end{aligned}$$

Reflection and Transmission Coefficients

$$\Gamma = \frac{E_0^r}{E_0^i} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} \quad (\text{normal incidence}),$$
$$\tau = \frac{E_0^t}{E_0^i} = \frac{2\eta_2}{\eta_2 + \eta_1} \quad (\text{normal incidence}).$$

$$\tau = 1 + \Gamma \quad (\text{normal incidence}).$$

For non-magnetic, low-loss media:

$$\Gamma = \frac{\sqrt{\epsilon_{r1}} - \sqrt{\epsilon_{r2}}}{\sqrt{\epsilon_{r1}} + \sqrt{\epsilon_{r2}}} = \frac{n_1 - n_2}{n_1 + n_2}; \quad \tau = \frac{2n_1}{n_1 + n_2}$$

Where $n = \frac{c}{v_p} = \sqrt{\mu_r \epsilon_r} = \sqrt{\epsilon_r}$ is the refractive index.

General

When $\mu_r = 1$

Note: $n \neq \eta$!

Summary: EM Fields for Normal Incidence

Incident Wave

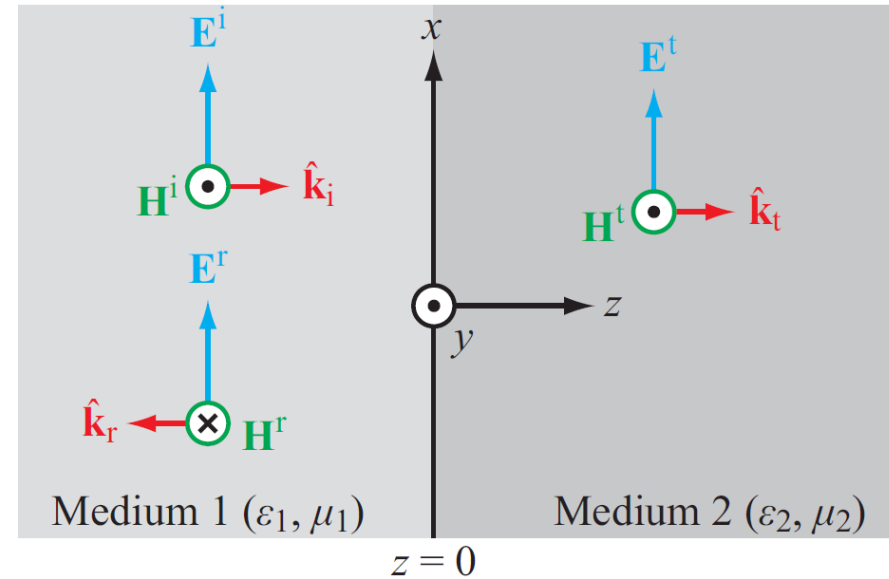
$$\mathbf{E}^i = E^i e^{-jk_1 z} \hat{\mathbf{x}}$$
$$\mathbf{H}^i = (E^i / \eta_1) e^{-jk_1 z} \hat{\mathbf{y}}$$

Reflected Wave

$$\mathbf{E}^r = \Gamma E^i e^{+jk_1 z} \hat{\mathbf{x}}$$
$$\mathbf{H}^r = -(\Gamma E^i / \eta_1) e^{+jk_1 z} \hat{\mathbf{y}}$$

Coefficients

$$\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} ; \quad \tau = \frac{2\eta_2}{\eta_2 + \eta_1} ; \quad k = \omega \sqrt{\mu \epsilon}$$



Transmitted Wave

$$\mathbf{E}^t = \tau E^i e^{-jk_2 z} \hat{\mathbf{x}}$$
$$\mathbf{H}^t = (\tau E^i / \eta_2) e^{-jk_2 z} \hat{\mathbf{y}}$$

Example 1.

A 10 GHz wave, with amplitude 5 [V/m] travels in air in the +z-direction and forms normal incidence onto a piece of glass ($\mu_r = 1$; $\epsilon_r = 2.25$; $\sigma = 0$). The E-field is linearly polarized in the x-direction. Find the reflection and transmission coefficient; write the electric field and magnetic field in air and in glass.

Solution Steps: Find Γ and τ , Write $\mathbf{E}^i, \mathbf{E}^r = \Gamma \mathbf{E}^i, \mathbf{E}^t = \tau \mathbf{E}^i$, write $\mathbf{H}^i, \mathbf{H}^r = -\Gamma \mathbf{H}^i, \mathbf{H}^t = \tau \mathbf{H}^i$.

Solution:

$$\Gamma = \frac{n_1 - n_2}{n_1 + n_2} = \frac{1 - 1.5}{1 + 1.5} = -0.2; \quad \tau = \frac{2n_1}{n_1 + n_2} = 0.8$$

$$\eta_1 = 377 [\Omega]; \quad \eta_2 = \frac{377}{\sqrt{\epsilon_r}} = 251.3 [\Omega];$$

$$k_1 = 2\pi f \sqrt{\mu_0 \epsilon_0} = \frac{2\pi f}{c} = \frac{2\pi \times 10^{10}}{3 \times 10^8} = 209.4 [m^{-1}]; \quad k_2 = k_1 \sqrt{\mu_r \epsilon_r} = 314.1 [m^{-1}]$$

Example 1 Cont'd

$$\mathbf{E}^i = 5e^{-jk_1z} \hat{\mathbf{x}} \quad \mathbf{H}^i = \frac{1}{\eta_1} \hat{\mathbf{k}} \times \mathbf{E}^i = \frac{5}{377} e^{-jk_1z} \hat{\mathbf{y}} \\ = 13.26e^{-jk_1z} \hat{\mathbf{y}} \text{ [mA/m]}$$

$$\mathbf{E}^r = -1e^{+jk_1z} \hat{\mathbf{x}} \quad \mathbf{H}^r = 2.652e^{+jk_1z} \hat{\mathbf{y}} \text{ [mA/m]}$$

$$\mathbf{E}^t = 4e^{-jk_2z} \hat{\mathbf{x}} \quad \mathbf{H}^t = 10.61e^{-jk_2z} \hat{\mathbf{y}} \text{ [mA/m]}$$

(You should substitute in k_1 and k_2 into your answers.)

Example 8-3: Normal Incidence on a Metal Surface

A 1-GHz x -polarized plane wave traveling in the $+z$ -direction is incident from air upon a copper surface. The air-to-copper interface is at $z = 0$ and copper has $\epsilon_r = 1$, $\mu_r = 1$, and $\sigma = 5.8 \times 10^7$ S/m. If the amplitude of the electric field of the incident wave is 12 (mV/m), obtain expressions for the instantaneous electric and magnetic fields in the air medium. Assume the metal surface to be several skin depths deep.

Solution: In medium 1 (air), $\alpha = 0$,

$$\beta = k_1 = \frac{\omega}{c} = \frac{2\pi \times 10^9}{3 \times 10^8} = \frac{20\pi}{3} \quad (\text{rad/m}),$$

$$\eta_1 = \eta_0 = 377 \, (\Omega), \quad \lambda = \frac{2\pi}{k_1} = 0.3 \, \text{m}.$$

At $f = 1$ GHz, copper is an excellent conductor because

$$\frac{\epsilon''}{\epsilon'} = \frac{\sigma}{\omega \epsilon_r \epsilon_0} = \frac{5.8 \times 10^7}{2\pi \times 10^9 \times (10^{-9}/36\pi)} = 1 \times 10^9 \gg 1.$$

Cont.

Ulaby Example 8-3 (cont.)

$$\begin{aligned}\eta_{c_2} &= (1 + j) \sqrt{\frac{\pi f \mu}{\sigma}} \\ &= (1 + j) \left[\frac{\pi \times 10^9 \times 4\pi \times 10^{-7}}{5.8 \times 10^7} \right]^{1/2} \\ &= 8.25(1 + j) \quad (\text{m}\Omega).\end{aligned}$$

Since η_{c_2} is so small compared to $\eta_0 = 377 \text{ } (\Omega)$ for air, the copper surface acts, in effect, like a short circuit. Hence,

$$\Gamma = \frac{\eta_{c_2} - \eta_0}{\eta_{c_2} + \eta_0} \simeq -1.$$

Cont.

Ulaby Example 8-3 (cont.)

Upon setting $\Gamma = -1$

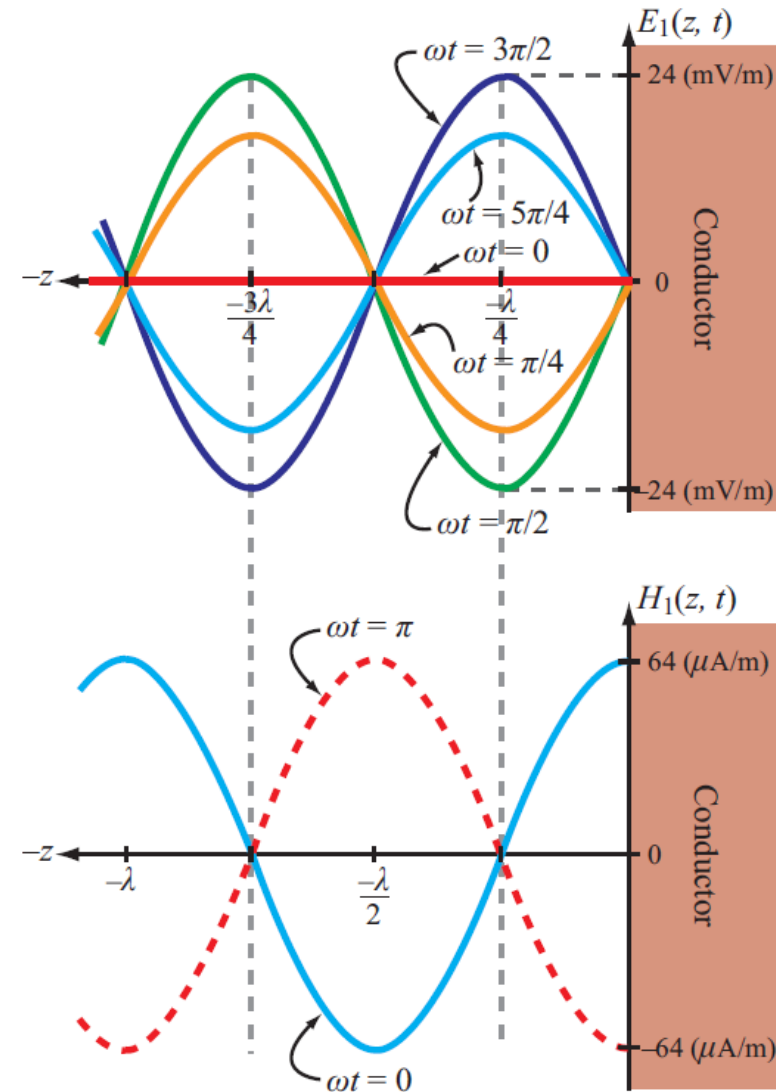
$$\begin{aligned}\tilde{\mathbf{E}}_1(z) &= \hat{\mathbf{x}} E_0^i (e^{-jk_1 z} - e^{jk_1 z}) \\ &= -\hat{\mathbf{x}} j 2 E_0^i \sin k_1 z,\end{aligned}$$

$$\begin{aligned}\tilde{\mathbf{H}}_1(z) &= \hat{\mathbf{y}} \frac{E_0^i}{\eta_1} (e^{-jk_1 z} + e^{jk_1 z}) \\ &= \hat{\mathbf{y}} 2 \frac{E_0^i}{\eta_1} \cos k_1 z.\end{aligned}$$

With $E_0^i = 12$ (mV/m), the instantaneous fields associated with these phasors are

$$\begin{aligned}\mathbf{E}_1(z, t) &= \Re\{\tilde{\mathbf{E}}_1(z) e^{j\omega t}\} \\ &= \hat{\mathbf{x}} 2 E_0^i \sin k_1 z \sin \omega t \\ &= \hat{\mathbf{x}} 24 \sin(20\pi z/3) \sin(2\pi \times 10^9 t) \quad (\text{mV/m}),\end{aligned}$$

$$\begin{aligned}\mathbf{H}_1(z, t) &= \Re\{\tilde{\mathbf{H}}_1(z) e^{j\omega t}\} \\ &= \hat{\mathbf{y}} 2 \frac{E_0^i}{\eta_1} \cos k_1 z \cos \omega t \\ &= \hat{\mathbf{y}} 64 \cos(20\pi z/3) \cos(2\pi \times 10^9 t) \quad (\mu\text{A/m}).\end{aligned}$$



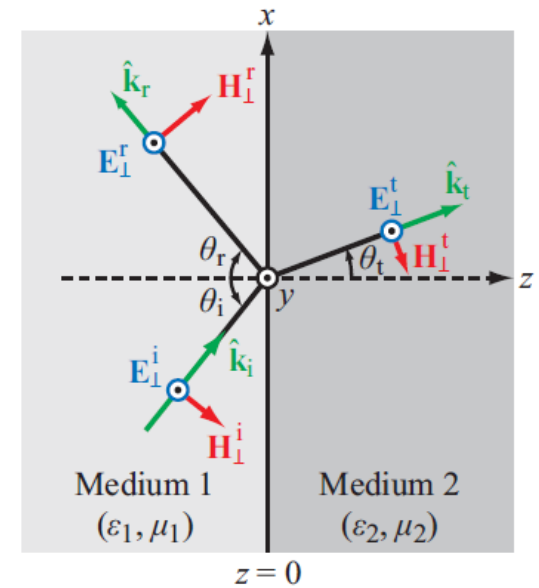
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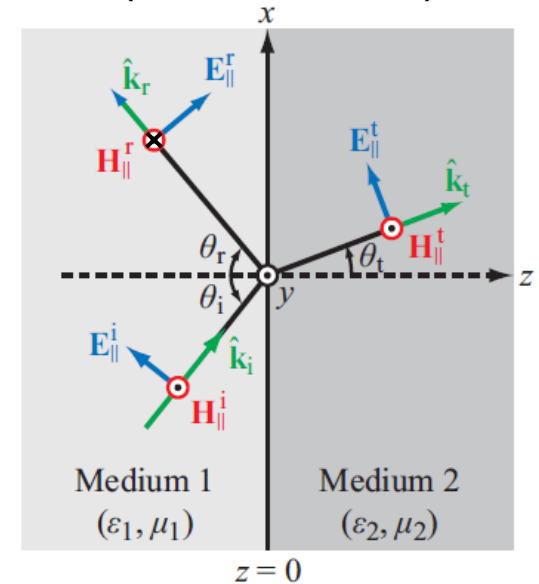
Oblique Incidence

Plane of incidence is defined as the plane containing the normal to the boundary and the direction of propagation of the incident wave (x - z plane in the figure).

A wave of arbitrary polarization may be described as the superposition of two orthogonally polarized waves, one with its electric field parallel to the plane of incidence (**parallel polarization**) and the other with its electric field perpendicular to the plane of incidence (**perpendicular polarization**).



(a) Perpendicular polarization
(TE Polarization)



(b) Parallel polarization
(TM Polarization)

Snell's Law

Consider the tangential E-field TM case:

$$\mathbf{E}_{tan}^i = \cos \theta_i E_0^i e^{-jk_{ix}x} \hat{\mathbf{x}}$$

$$\mathbf{E}_{tan}^r = \cos \theta_r E_0^r e^{-jk_{rx}x} \hat{\mathbf{x}}$$

$$\mathbf{E}_{tan}^t = \cos \theta_t E_0^t e^{-jk_{tx}x} \hat{\mathbf{x}}$$

$$k_{ix} = k_1 \sin \theta_i$$

$$k_{rx} = k_1 \sin \theta_r$$

$$k_{tx} = k_2 \sin \theta_t$$

$$\mathbf{E}_{tan}^i + \mathbf{E}_{tan}^r = \mathbf{E}_{tan}^t \Rightarrow C_{1i}e^{-jk_{ix}x} + C_{1r}e^{-jk_{rx}x} = C_2e^{-jk_{tx}x}$$

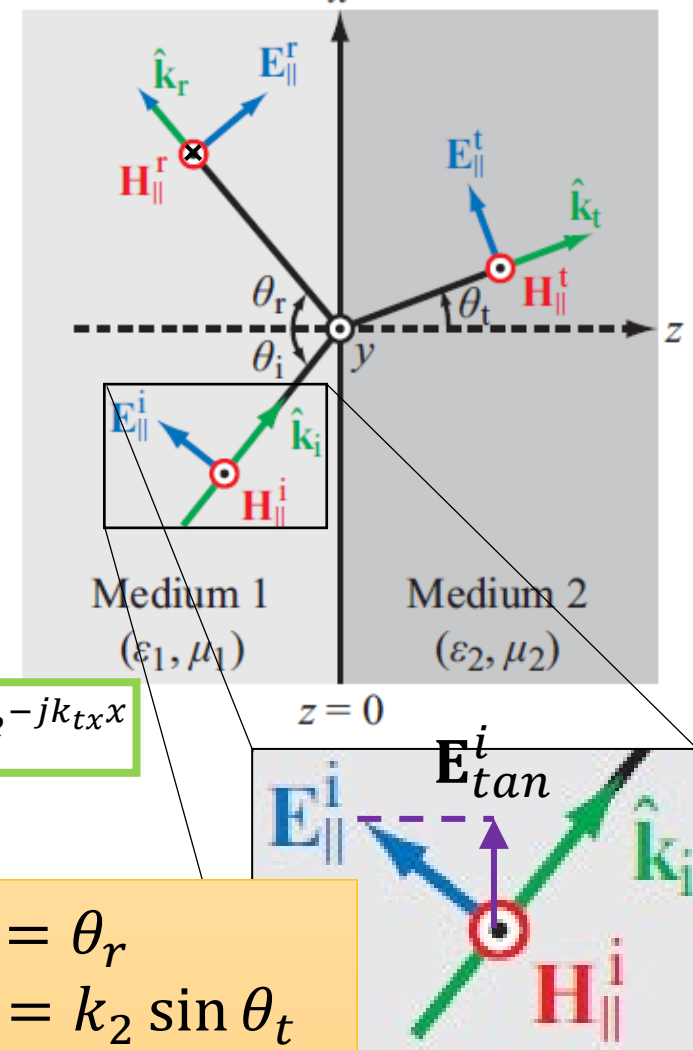
(Must be true for all x)

From and :

$$k_{ix} = k_{rx} = k_{tx} \Rightarrow$$

$$\begin{aligned} \theta_i &= \theta_r \\ k_1 \sin \theta_i &= k_2 \sin \theta_t \\ (\text{or } n_1 \sin \theta_i &= n_2 \sin \theta_t) \end{aligned}$$

TM Polarization



(Snell's Law)

Critical Angle

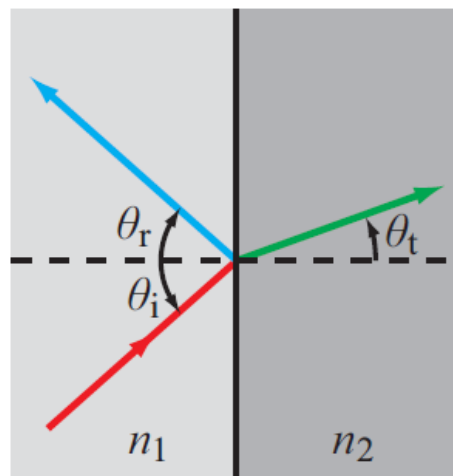
Snell's Law:

$$\theta_i = \theta_r$$
$$n_1 \sin \theta_i = n_2 \sin \theta_t$$

When the refraction angle is 90° , the corresponding incidence angle is called the **critical angle**.

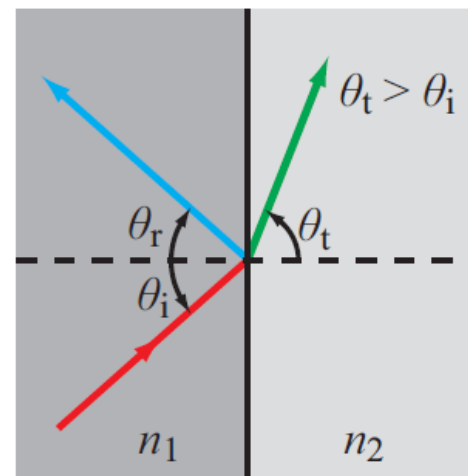
$$\sin \theta_c = \frac{n_2}{n_1} \sin \theta_t \Big|_{\theta_t = \pi/2} = \frac{n_2}{n_1}$$
$$= \sqrt{\frac{\epsilon_{r2}}{\epsilon_{r1}}} \quad (\text{for } \mu_1 = \mu_2).$$

Inward refraction



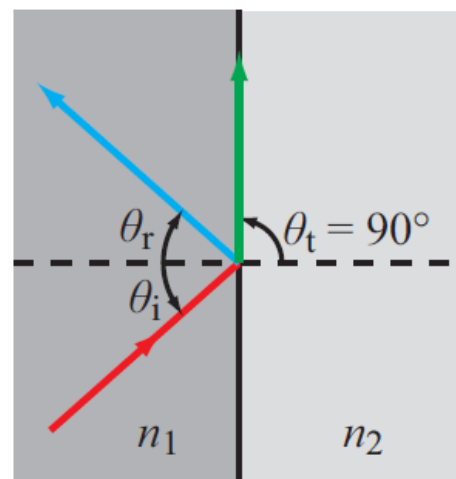
(a) $n_1 < n_2$

Outward refraction



(b) $n_1 > n_2$

No transmission



(c) $n_1 > n_2$ and $\theta_i = \theta_c$

Example 8-4: Light Beam Passing through a Slab

A dielectric slab with index of refraction n_2 is surrounded by a medium with index of refraction n_1 , as shown in Fig. 8-11. If $\theta_i < \theta_c$, show that the emerging beam is parallel to the incident beam.

Solution: At the slab's upper surface, Snell's law gives

$$\sin \theta_2 = \frac{n_1}{n_2} \sin \theta_1$$

and, similarly, at the slab's lower surface,

$$\sin \theta_3 = \frac{n_2}{n_3} \sin \theta_2 = \frac{n_2}{n_1} \sin \theta_2.$$

Substituting Eq. (8.33) into Eq. (8.34) gives

$$\sin \theta_3 = \left(\frac{n_2}{n_1} \right) \left(\frac{n_1}{n_2} \right) \sin \theta_1 = \sin \theta_1.$$

Hence, $\theta_3 = \theta_1$. The slab displaces the beam's position, but the beam's direction remains unchanged.

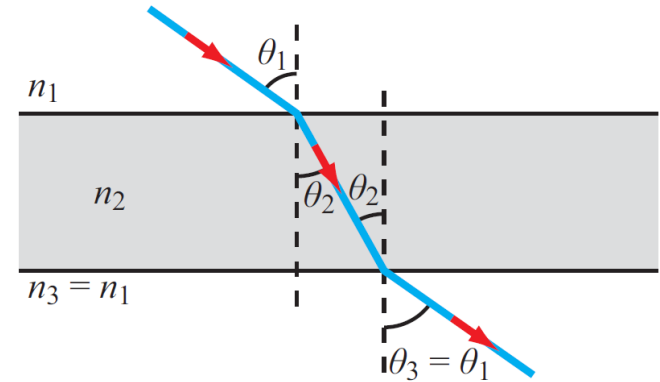


Figure 8-11: The exit angle θ_3 is equal to the incidence angle θ_1 if the dielectric slab has parallel boundaries and is surrounded by media with the same index of refraction on both sides (Example 8-4).

Oblique Incidence for TE Polarization

Notation:

$$k_i = k_r = k_1; \quad k_t = k_2$$

$$\theta_i = \theta_r = \theta_1; \quad \theta_t = \theta_2$$

Plane Waves (Signs read from diagram)

$$\mathbf{E}^i = E_0^i e^{-j(k_{1x}x + k_{1z}z)} \hat{\mathbf{y}} = E_y^i \hat{\mathbf{y}} \quad \mathbf{H}^i = (E_y^i / \eta_1) (-\cos \theta_1 \hat{\mathbf{x}} + \sin \theta_1 \hat{\mathbf{z}})$$

$$\mathbf{E}^r = E_0^r e^{-j(k_{1x}x - k_{1z}z)} \hat{\mathbf{y}} = E_y^r \hat{\mathbf{y}} \quad \mathbf{H}^r = (E_y^r / \eta_1) (\cos \theta_1 \hat{\mathbf{x}} + \sin \theta_1 \hat{\mathbf{z}})$$

$$\mathbf{E}^t = E_0^t e^{-j(k_{2x}x + k_{2z}z)} \hat{\mathbf{y}} = E_y^t \hat{\mathbf{y}} \quad \mathbf{H}^t = (E_y^t / \eta_2) (-\cos \theta_2 \hat{\mathbf{x}} + \sin \theta_2 \hat{\mathbf{z}})$$

$$k_{1x} = k_1 \sin \theta_1$$

$$k_{2x} = k_2 \sin \theta_2$$

$$k_{1z} = k_1 \cos \theta_1$$

$$k_{2z} = k_2 \cos \theta_2$$

Tangential Components at $z = 0$

$$\mathbf{E}_{tan}^i = E_0^i e^{-jk_{1x}x} \hat{\mathbf{y}} \quad \mathbf{H}_{tan}^i = -(\cos \theta_1 / \eta_1) E_0^i e^{-jk_{1x}x} \hat{\mathbf{x}}$$

$$\mathbf{E}_{tan}^r = E_0^r e^{-jk_{1x}x} \hat{\mathbf{y}} \quad \mathbf{H}_{tan}^r = (\cos \theta_1 / \eta_1) E_0^r e^{-jk_{1x}x} \hat{\mathbf{x}}$$

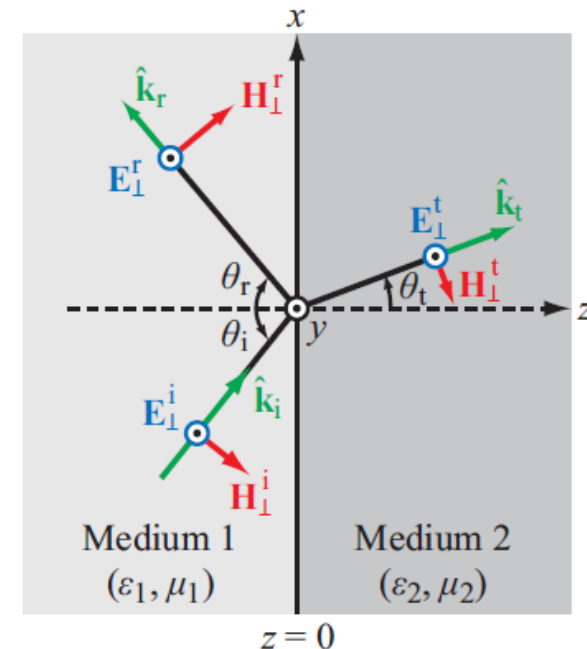
$$\mathbf{E}_{tan}^t = E_0^t e^{-jk_{2x}x} \hat{\mathbf{y}} \quad \mathbf{H}_{tan}^t = -(\cos \theta_2 / \eta_2) E_0^t e^{-jk_{2x}x} \hat{\mathbf{x}}$$

Boundary Conditions

$$k_{1x} = k_{2x} = k_x;$$

$$\mathbf{E}_{tan}^i + \mathbf{E}_{tan}^r = \mathbf{E}_{tan}^t;$$

$$\mathbf{H}_{tan}^i + \mathbf{H}_{tan}^r = \mathbf{H}_{tan}^t.$$



(a) Perpendicular polarization
(TE Polarization)

Oblique Incidence for TE Polarization

Substitute E and H fields into B.C.'s to get:

$$E_0^i + E_0^r = E_0^t$$

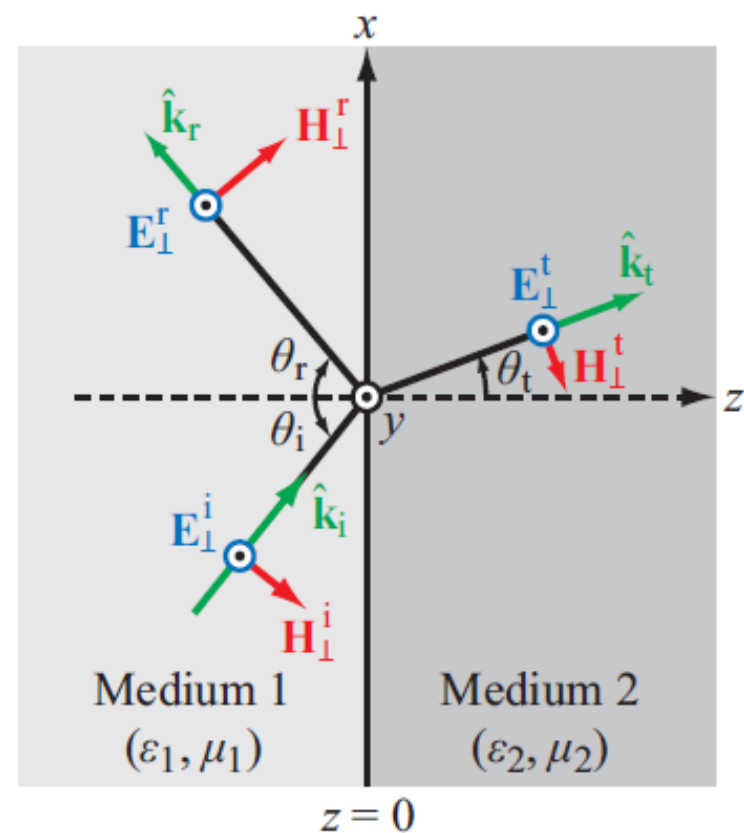
$$\frac{\cos \theta_1}{\eta_1} E_0^i - \frac{\cos \theta_1}{\eta_1} E_0^r = \frac{\cos \theta_2}{\eta_2} E_0^t$$

Rearrange to get:

$$\frac{E_0^r}{E_0^i} \equiv \Gamma_{TE} = \frac{\eta_2 \cos \theta_1 - \eta_1 \cos \theta_2}{\eta_2 \cos \theta_1 + \eta_1 \cos \theta_2} ;$$

$$\frac{E_0^t}{E_0^i} \equiv \tau_{TE} = \frac{2\eta_2 \cos \theta_1}{\eta_2 \cos \theta_1 + \eta_1 \cos \theta_2} .$$

(You can do the same for the TM polarization)



(a) Perpendicular polarization
(TE Polarization)

Oblique Incidence

TE Polarization:

$$\Gamma_{\text{TE}} = \frac{\eta_2 \cos \theta_1 - \eta_1 \cos \theta_2}{\eta_2 \cos \theta_1 + \eta_1 \cos \theta_2} ;$$

$$\tau_{\text{TE}} = \frac{2\eta_2 \cos \theta_1}{\eta_2 \cos \theta_1 + \eta_1 \cos \theta_2} ;$$

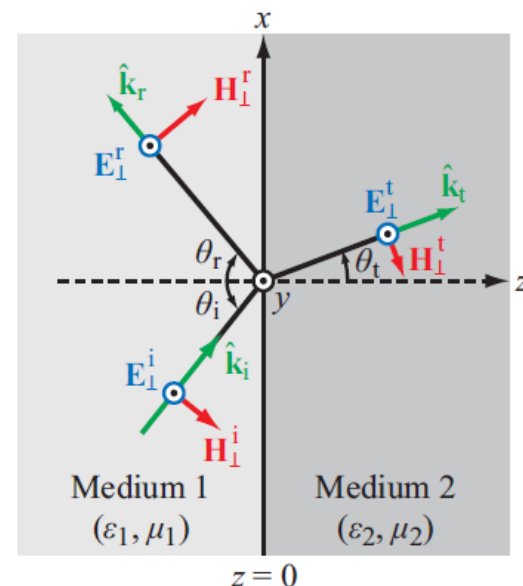
$$\tau_{\text{TE}} = 1 + \Gamma_{\text{TE}} .$$

TM Polarization:

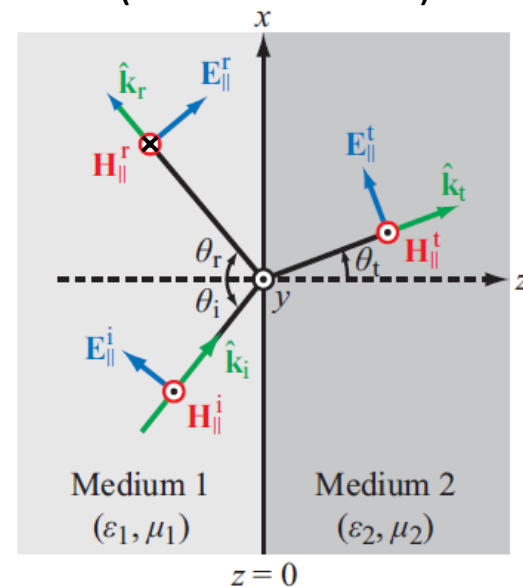
$$\Gamma_{\text{TM}} = \frac{\eta_2 \cos \theta_2 - \eta_1 \cos \theta_1}{\eta_2 \cos \theta_2 + \eta_1 \cos \theta_1} ;$$

$$\tau_{\text{TM}} = \frac{2\eta_2 \cos \theta_1}{\eta_2 \cos \theta_2 + \eta_1 \cos \theta_1} ;$$

$$\tau_{\text{TM}} = (1 + \Gamma_{\text{TM}}) \frac{\cos \theta_1}{\cos \theta_2} .$$



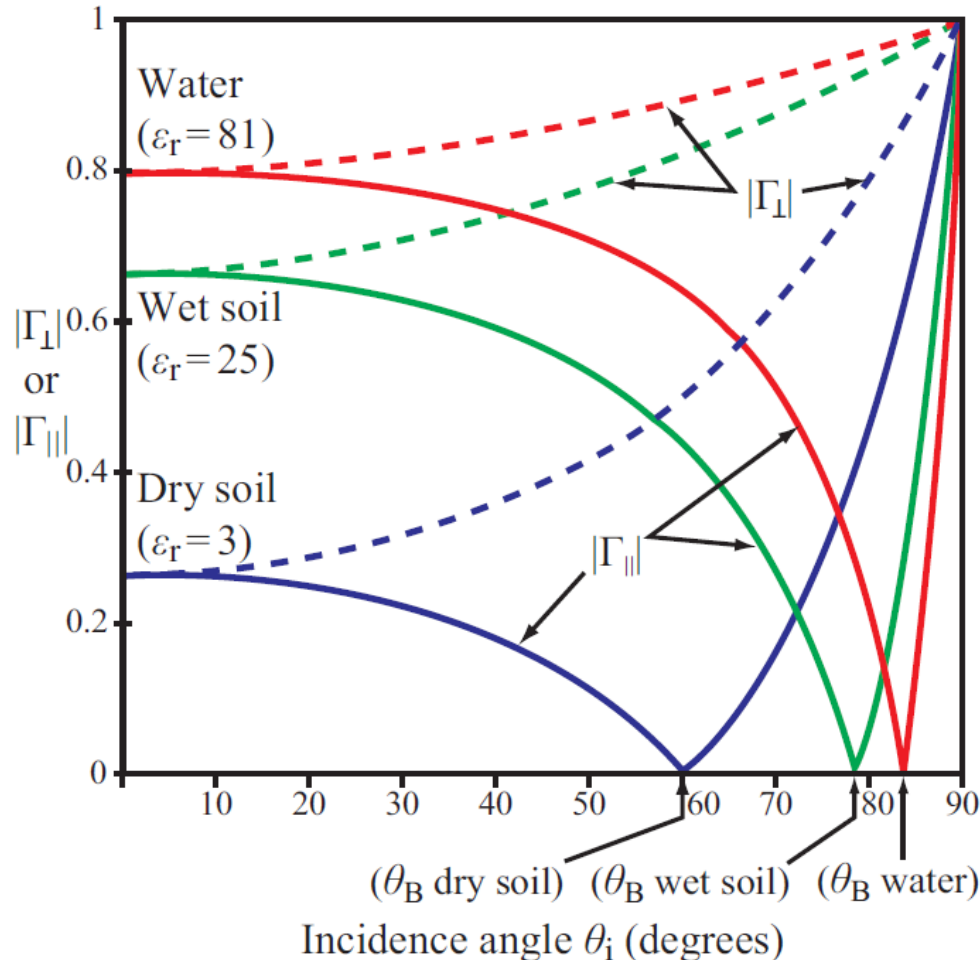
(a) Perpendicular polarization
(**TE** Polarization)



(b) Parallel polarization
(**TM** Polarization)

Reflection Coefficient vs. Angle

Ulaby Fig. 8-17.



$$\Gamma_{TE} = \frac{\eta_2 \cos \theta_1 - \eta_1 \cos \theta_2}{\eta_2 \cos \theta_1 + \eta_1 \cos \theta_2} ;$$

$$\Gamma_{TM} = \frac{\eta_2 \cos \theta_2 - \eta_1 \cos \theta_1}{\eta_2 \cos \theta_2 + \eta_1 \cos \theta_1} .$$

Brewster Angle

The Brewster angle θ_B is defined as the incidence angle θ_i at which the Fresnel reflection coefficient $\Gamma = 0$.

Perpendicular Polarization

$\theta_{B\perp}$ *does not exist for nonmagnetic materials.* (Why?)

Parallel Polarization

$$\begin{aligned}\theta_{B\parallel} &= \sin^{-1} \sqrt{\frac{1}{1 + (\varepsilon_1/\varepsilon_2)}} \\ &= \tan^{-1} \sqrt{\frac{\varepsilon_2}{\varepsilon_1}} \quad (\text{for } \mu_1 = \mu_2).\end{aligned}$$

Summary For Reflection and Transmission

Table 8-2: Expressions for Γ , τ , R , and T for wave incidence from a medium with intrinsic impedance η_1 onto a medium with intrinsic impedance η_2 . Angles θ_i and θ_t are the angles of incidence and transmission, respectively.

Property	Normal Incidence $\theta_i = \theta_t = 0$	Perpendicular Polarization	Parallel Polarization
Reflection coefficient	$\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$	$\Gamma_{\perp} = \frac{\eta_2 \cos \theta_i - \eta_1 \cos \theta_t}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$	$\Gamma_{\parallel} = \frac{\eta_2 \cos \theta_t - \eta_1 \cos \theta_i}{\eta_2 \cos \theta_t + \eta_1 \cos \theta_i}$
Transmission coefficient	$\tau = \frac{2\eta_2}{\eta_2 + \eta_1}$	$\tau_{\perp} = \frac{2\eta_2 \cos \theta_i}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$	$\tau_{\parallel} = \frac{2\eta_2 \cos \theta_i}{\eta_2 \cos \theta_t + \eta_1 \cos \theta_i}$
Relation of Γ to τ	$\tau = 1 + \Gamma$	$\tau_{\perp} = 1 + \Gamma_{\perp}$	$\tau_{\parallel} = (1 + \Gamma_{\parallel}) \frac{\cos \theta_i}{\cos \theta_t}$
Reflectivity	$R = \Gamma ^2$	$R_{\perp} = \Gamma_{\perp} ^2$	$R_{\parallel} = \Gamma_{\parallel} ^2$
Transmissivity	$T = \tau ^2 \left(\frac{\eta_1}{\eta_2} \right)$	$T_{\perp} = \tau_{\perp} ^2 \frac{\eta_1 \cos \theta_t}{\eta_2 \cos \theta_i}$	$T_{\parallel} = \tau_{\parallel} ^2 \frac{\eta_1 \cos \theta_t}{\eta_2 \cos \theta_i}$
Relation of R to T	$T = 1 - R$	$T_{\perp} = 1 - R_{\perp}$	$T_{\parallel} = 1 - R_{\parallel}$
Notes: (1) $\sin \theta_t = \sqrt{\mu_1 \epsilon_1 / \mu_2 \epsilon_2} \sin \theta_i$; (2) $\eta_1 = \sqrt{\mu_1 / \epsilon_1}$; (3) $\eta_2 = \sqrt{\mu_2 / \epsilon_2}$; (4) for nonmagnetic media, $\eta_2 / \eta_1 = n_1 / n_2$.			

Summary

- In this class, we considered how plane waves behave in the presence of a boundary
 - We showed how plane waves reflect and refract
 - We calculated the electromagnetic field across the reflection boundary
 - We proved Snell's Law, examined the critical angle and the Brewster angle.

Light Propagation with Phase Discontinuities: Generalized Laws of Reflection and Refraction

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Conventional optical components rely on gradual phase shifts accumulated during light propagation to shape light beams. New degrees of freedom are attained by introducing abrupt phase changes over the scale of the wavelength. A two-dimensional array of optical resonators with spatially varying phase response and subwavelength separation can imprint such phase discontinuities on propagating light as it traverses the interface between two media. Anomalous reflection and refraction phenomena are observed in this regime in optically thin arrays of metallic antennas on silicon with a linear phase variation along the interface, which are in excellent agreement with generalized laws derived from Fermat's principle. Phase discontinuities provide great flexibility in the design of light beams, as illustrated by the generation of optical vortices through use of planar designer metallic interfaces.

The shaping of the wavefront of light with optical components such as lenses and prisms, as well as diffractive elements such as gratings and holograms, relies on gradual phase changes accumulated along the optical path. This approach is generalized in transformation optics (1, 2), which uses metamaterials to bend light in unusual ways, achieving such phenomena as negative refraction, subwavelength-focusing, and cloaking (3, 4) and even to explore unusual geometries of space-time in the early universe (5). A new degree of freedom of controlling wavefronts can be attained by introducing abrupt phase shifts over the scale of the wavelength along the optical path, with the propagation of light governed by Fermat's principle. The latter states that

between two media; $\Phi(\vec{r}_s)$ depends on the coordinate $\vec{r}_s$ along the interface. Then, the total phase shift $\Phi(\vec{r}_s) + \int_A^B \vec{k} \cdot d\vec{r}$ will be stationary for the actual path that light takes; $\vec{k}$ is the wave vector of the propagating light. This provides a generalization of the laws of reflection and refraction, which is applicable to a wide range of subwavelength structured interfaces between two media throughout the optical spectrum.

Generalized laws of reflection and refraction. The introduction of an abrupt phase shift, denoted as phase discontinuity, at the interface between two media allows us to revisit the laws of reflection and refraction by applying Fermat's principle. Consider an incident plane wave at an angle θ_i . Assuming that the two paths are infi-

gles for total internal reflection, provided that $n_t < n_i$:

$$\theta_c = \arcsin\left(\pm \frac{n_t}{n_i} - \frac{\lambda_0}{2\pi n_i} \frac{d\Phi}{dx}\right) \quad (3)$$

Similarly, for reflection we have

$$\sin(\theta_r) - \sin(\theta_i) = \frac{\lambda_0}{2\pi n_i} \frac{d\Phi}{dx} \quad (4)$$

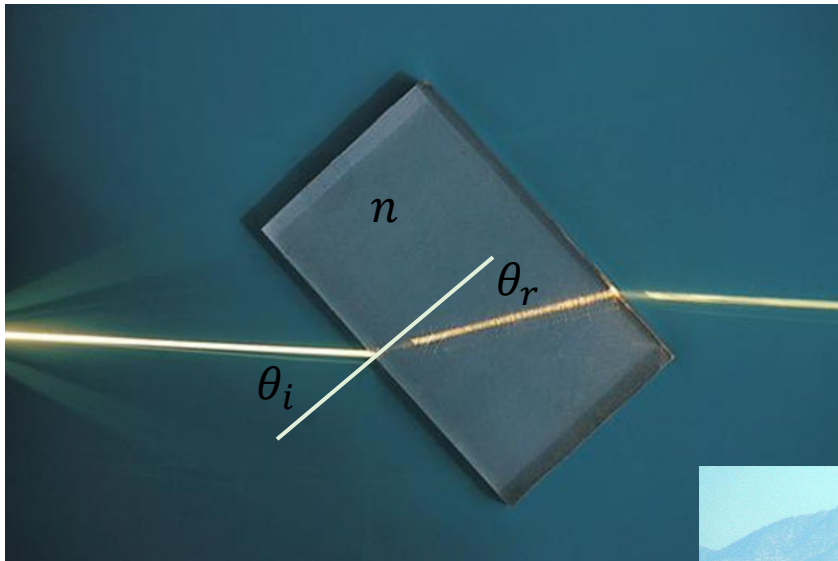
where θ_r is the angle of reflection. There is a nonlinear relation between θ_r and θ_i , which is markedly different from conventional specular reflection. Equation 4 predicts that there is always a critical angle of incidence

$$\theta'_c = \arcsin\left(1 - \frac{\lambda_0}{2\pi n_i} \left|\frac{d\Phi}{dx}\right|\right) \quad (5)$$

above which the reflected beam becomes evanescent.

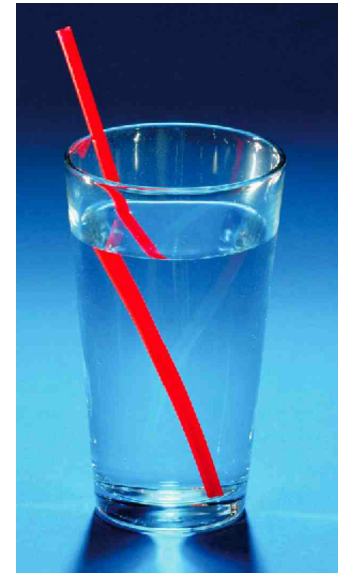
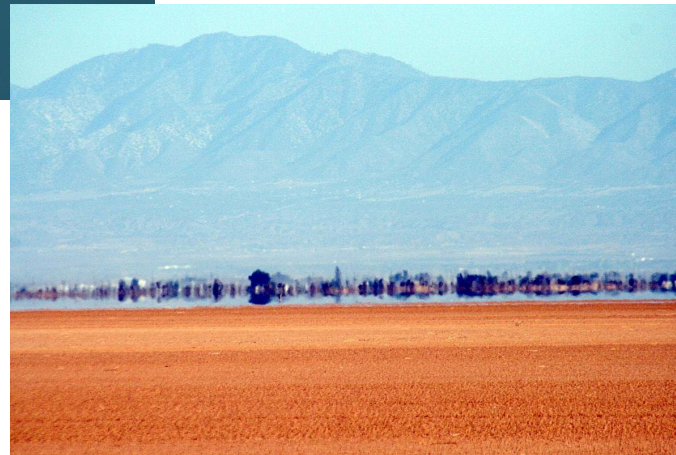
In the above derivation, we have assumed that Φ is a continuous function of the position along the interface; thus, all the incident energy is transferred into the anomalous reflection and refraction. However, because experimentally we use an array of optically thin resonators with subwavelength separation to achieve the phase change along the interface, this discreteness implies that there are also regularly reflected and refracted beams, which follow conventional laws of reflection and refraction ($d\Phi/dx = 0$ in Eqs. 2 and 4). The separation between the resonators controls the amount of energy in the anomalously reflected and refracted beams. We have also assumed that the amplitudes of the scattered radiation by each resonator are identical, so that the reflected and refracted beams are plane waves. In the next section, we will show with simulations—which represent numerical solutions of Maxwell's

Snell's Law: Bending Light with Material

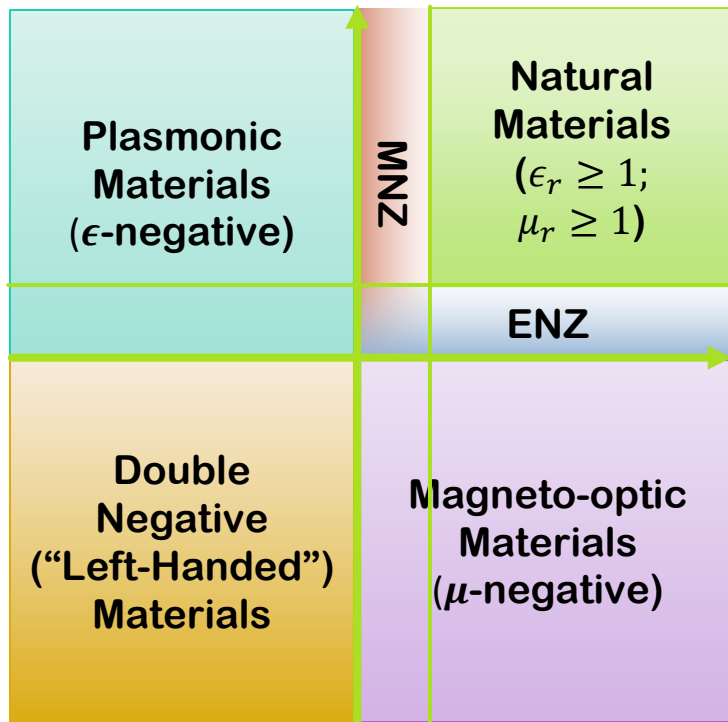


$$\sin \theta_i = n \sin \theta_r$$

($n \cong 1.5$ for glass)



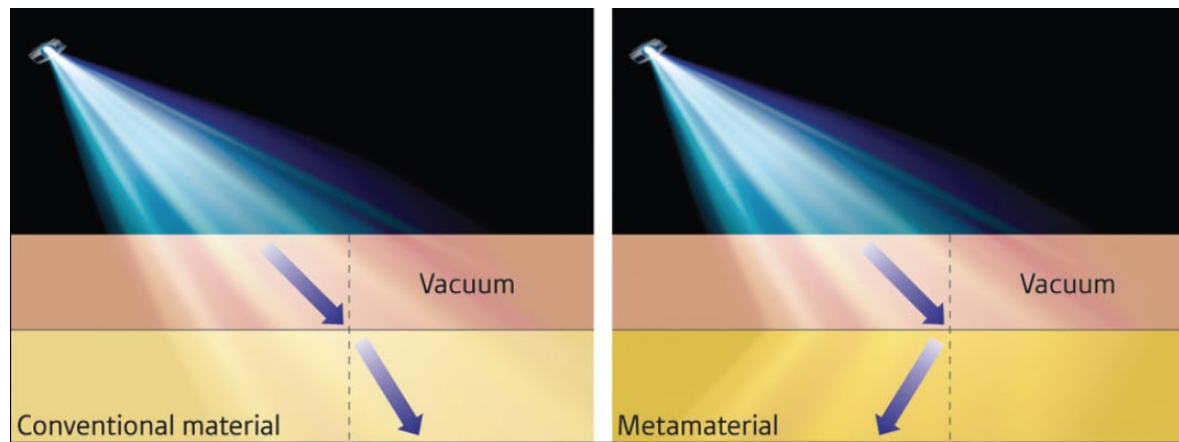
Metamaterials



- **Permittivity (ϵ , “epsilon”)** and **permeability (μ , “mu”)** denote a material’s response to **electric** and **magnetic** fields
- By engineering the material structure, one can achieve material properties unfound in nature

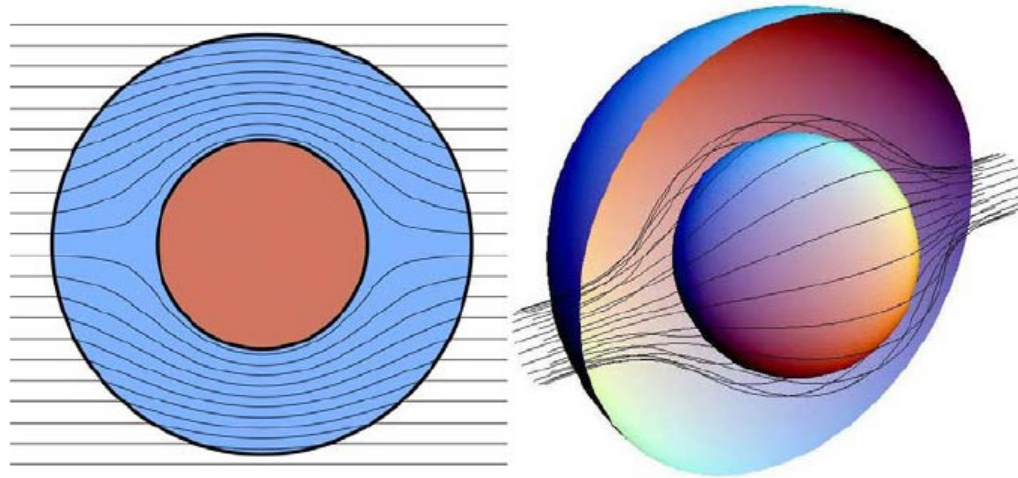
Negative refraction effects

- Weird things happen with light propagation in double negative materials (a.k.a. negative refractive index materials)



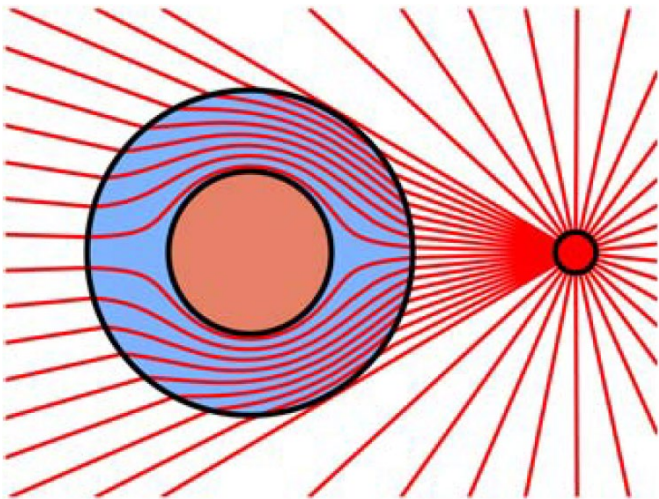
Electromagnetic Cloaking

- If we can make materials at will, we can also bend EM waves at will....



Pendry et. al., Science, vol.312, p.1780, 2006

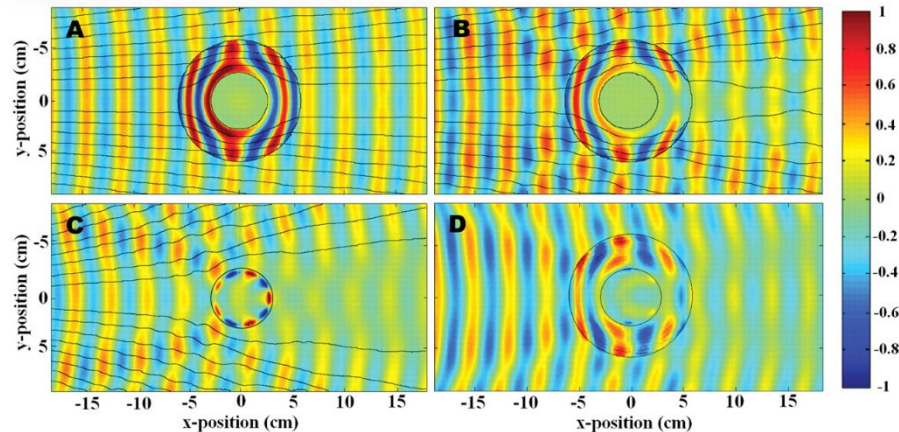
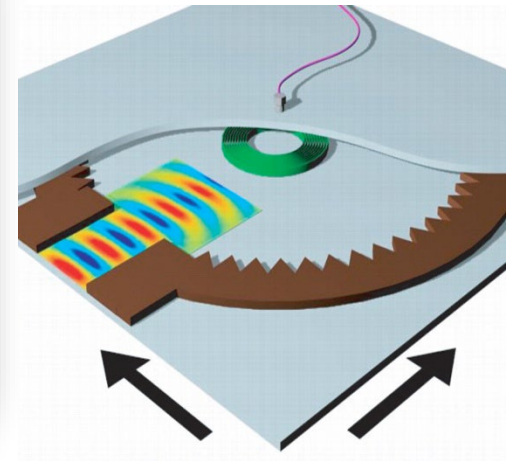
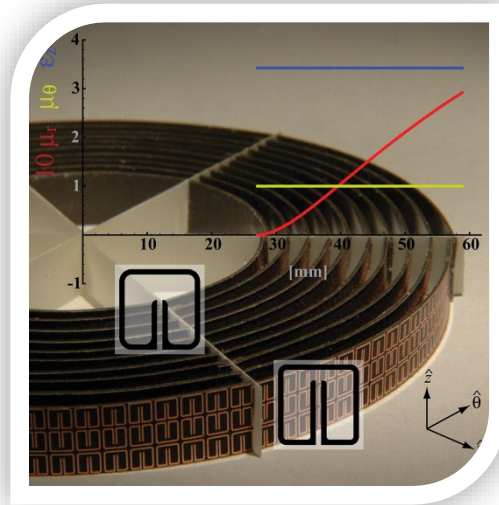
From idea to reality



$$\varepsilon'_{r'} = \mu'_{r'} = \frac{R_2}{R_2 - R_1} \frac{(r' - R_1)^2}{r'^2},$$

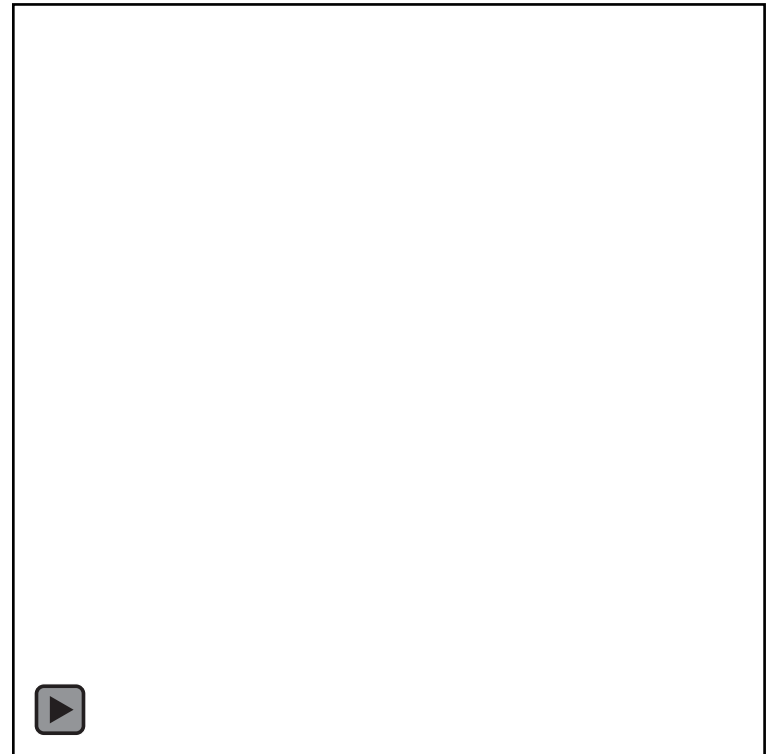
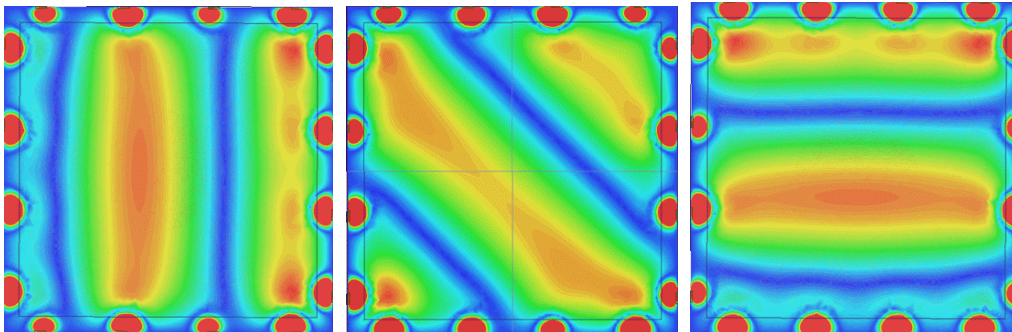
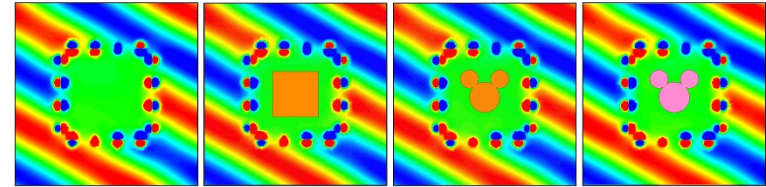
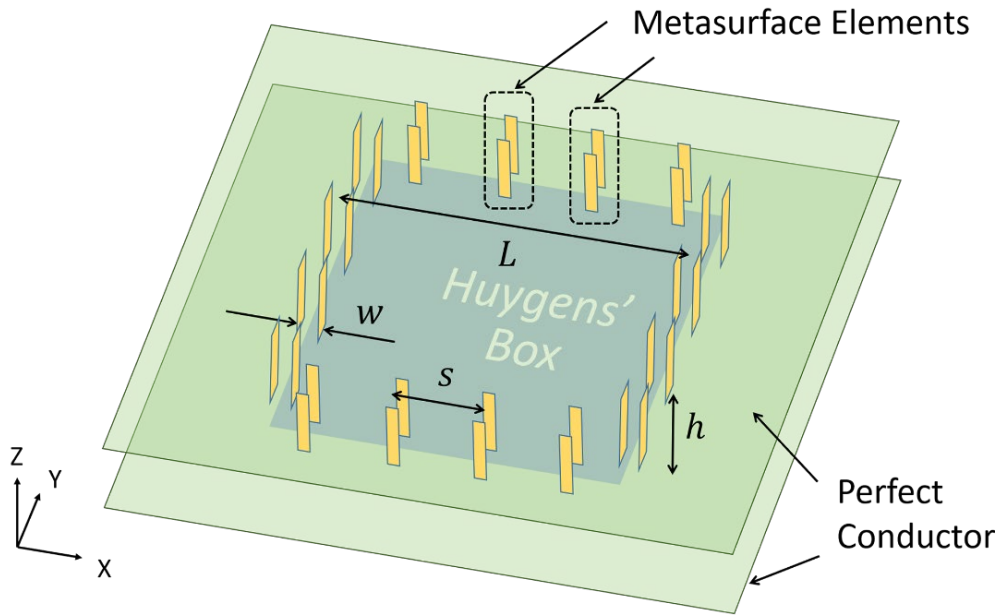
$$\varepsilon'_{\theta'} = \mu'_{\theta'} = \frac{R_2}{R_2 - R_1},$$

$$\varepsilon'_{\phi'} = \mu'_{\phi'} = \frac{R_2}{R_2 - R_1}$$



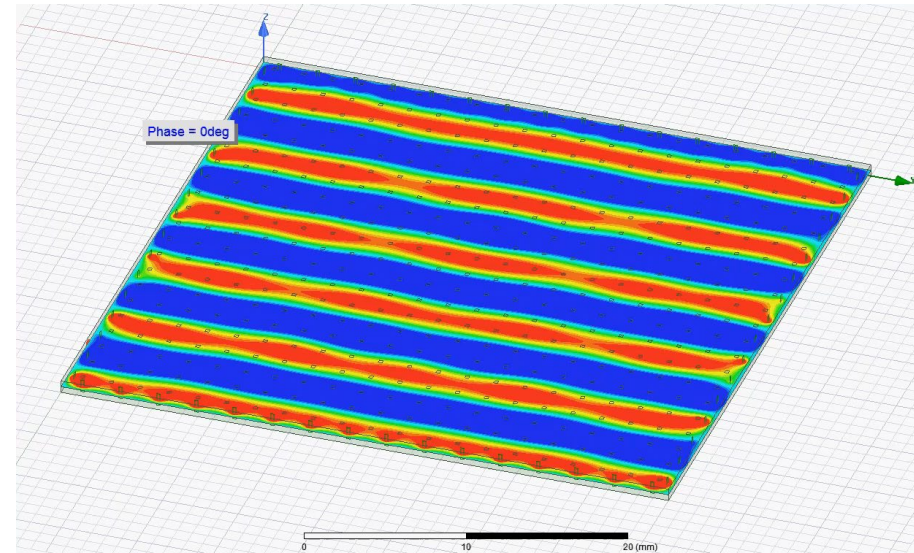
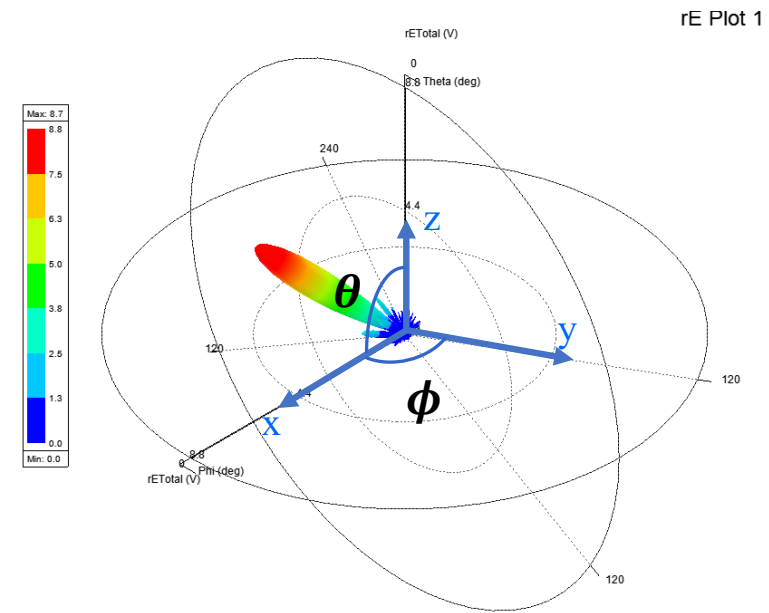
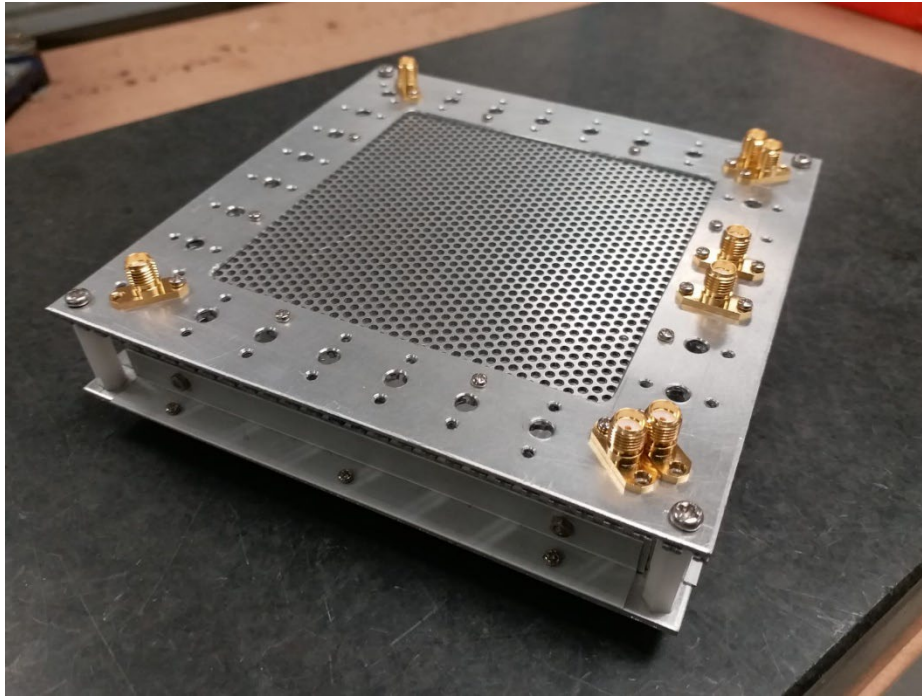
Pendry et al., Science, vol.312, p.1780, 2006; Schurig et al., Science, vol. 314, p. 977, 2006.

Active Cloaking with a Huygens' Box



Wong and Eleftheriades, IEEE TAP, Aug. 2020.

The Huygens' Box Antenna



K.A. Oyesina and A.M.H. Wong, IEEE AP-S, July 2019.

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K.A. Oyesina and A.M.H. Wong, IEEE AP-S, July 2022.